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Project Note

To	Fraser White and David Krushka TasWater
From	Suraj Neupane, Bill Cohen and Paul Southcott
Project	P514459-Waratah Dam Replacement Concept Designs
Project reference	E307175-P514459
Document number	ENTURA-FFD9B
Subject	Waratah Dam Replacement Concept Designs

Background

Waratah Dam has been found to be in very poor condition and not to meet dam safety compliance criteria in accordance with ANCOLD guidelines. The dam had a piping incident in 2017 and the reservoir level has been temporarily lowered down below the pipe hole to prevent failure of the dam. The flood capacity of the dam (pre 2017) was assessed to be approximately 1:400 AEP. The piping defect is assessed to be between the 1:2 and 1:5 AEP flood level. Ongoing operation of the dam in its current state is unacceptable due to the risks it poses and given the poor performance of the current dam remedial works are not considered to be good value. One alternative to reduce the risks is to replace the dam with a new structure constructed downstream of the existing dam.

TasWater has requested Entura to prepare concept designs for a compliant replacement embankment dam to the existing full supply level, as well as a design for an alternate concrete gravity weir with a full supply level approximately half the height of the existing dam.

Scope of work

The scope of work for the concept designs includes the following activities:

- Undertake a concept design of replacement embankment dam with the same full supply level (FSL) that would comply with prevailing ANCOLD guidelines, considering the replacement dam to be **High C** consequence category dam.
- Undertake a concept design of approximately 3m high concrete gravity weir that would comply with prevailing ANCOLD guidelines considering the weir to be a **Significant** consequence category dam.
- Prepare concept drawings for the replacement embankment and concrete gravity weir alternatives.

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- Undertake high level cost estimates ($\pm 50\%$) for replacement embankment and concrete gravity weir.
 - Prepare a brief report on the design (this project note).

Design Basis

Hydrology

Replacement embankment

Previous work on hydrology (Cohen & Southcott, 2018) had modelled inflows up to 1:2000 AEP (Annual Exceedance Probability) flowing into Waratah reservoir. For the replacement embankment, a design 1:10,000 AEP flood event were required to be compliant with **High C** fallback flood capacity requirement based on ANCOLD (2000) adopting the lower end of the required range.

In order to assess the required dam crest level for the proposed dam to safely pass a 1:10,000 AEP flood with the provided spillway, the following approach was applied:

- 1:10,000 AEP design rainfalls were developed:
 - Frequent and rare design rainfall depths (1:2,000 AEP and more frequent) with areal reduction factors (ARF) applied were obtained from the previous hydrology (Cohen & Southcott 2018)
 - Estimates of Probable Maximum Precipitation (PMP) design rainfall depths using the GSAM (Generalised Southeast Australia Method; BOM, 2006) for design storm durations of 24 hours and greater, and the GSDM (Generalised Short Duration Method; BOM 2003) for design storm durations of 6 hours and shorter. PMP depths between these durations were interpolated.
 - Estimates of rare (1:1,000 and 1:2,000 AEP) rainfalls for durations shorter than 24 hours were developed from 1:100 AEP rainfall depths using growth factors obtained from the 24 hour duration storm depths.
 - The 1:10,000 AEP design rainfall depths (Table 1) were interpolated using the method described by Australian Rainfall and Runoff (Book 8 Section 3.5.2.2; Ball et al 2016).
 - Extreme rainfall temporal patterns were obtained for short durations (Jordan et al 2005).
 - Extreme rainfall temporal patterns for longer durations were obtained from BoM (2006).
 - The existing uniform spatial pattern was unaltered.
- Losses developed by Entura (Cohen & Southcott, 2018) were further scaled down to the 1:10,000 AEP resulting in 0.69 mm initial loss and 0.69 mm/hour continuing loss.
- The model developed by Entura (Cohen & Southcott, 2018) was reinstated to run models, including the existing start storage level of RL 606.4m (0.1 m above FSL in the pre-2017 condition) and 0.5 m³/s base flow

- The model was reconfigured to use the newly designed 10m wide spillway which also has a FSL at RL 606.3m
- The model was run using an ensemble of temporal patterns for a range of design storm durations at the 1:10,000 AEP.

The results of the modelling (given in Figure 1) show that the **critical design storm duration for spill at Waratah Dam using the given configuration is approximately 18 hours or greater**. From visual inspection of results, the median estimates of peak level tend to plateau for longer durations. The worst case of those modelled is a 96 hour design storm, the longest duration modelled. Generally this may indicate that the critical duration may be longer than those analysed. However, given the small size of the reservoir’s catchment, and that the median values appear to plateau for durations greater than 18 hours, it is reasoned that if this is the case, the magnitude of increased level would be negligible. There is more variability in peak reservoir level due to temporal pattern than there is to design storm duration.

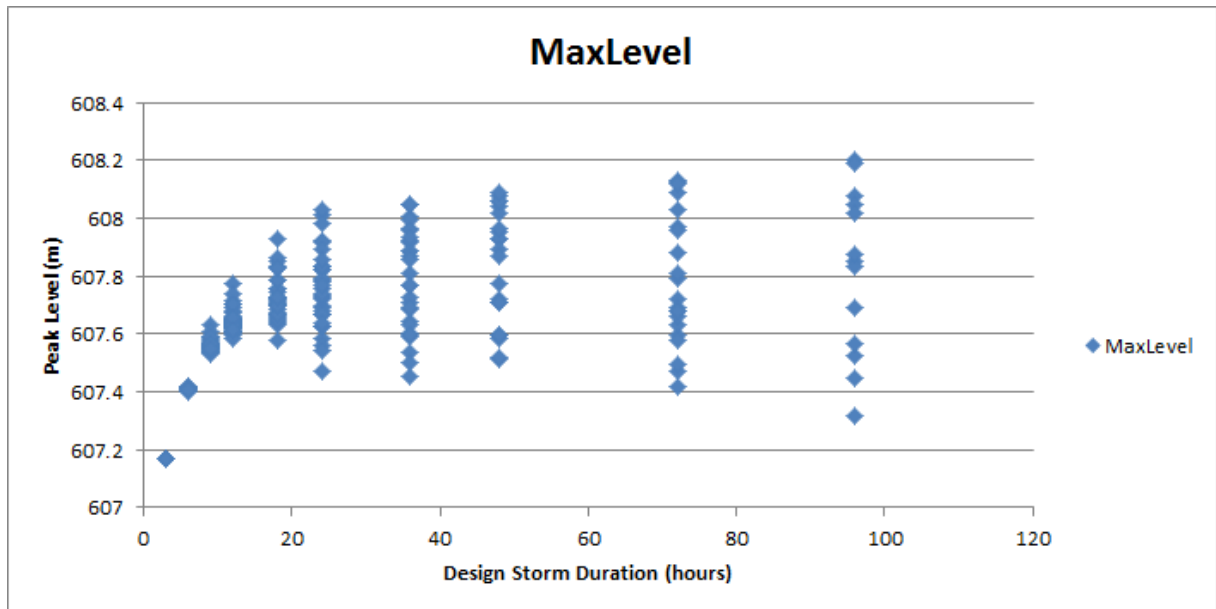


Figure 1 Peak level in Waratah Dam at the 1:10,000 AEP for a range of design storm durations and temporal patterns

For the 1:10,000 design flood, the median estimate of peak level is approximately RL 607.8m (spill of ~35m³/s). The worst case is RL 608.2 m (spill of ~ 50m³/s) for a 96 hour design storm simulation. The median spill estimate has been used to size the spillway for the replacement embankment.

Table 1: Design rainfall depths at the 1:10,000 AEP for the Waratah Dam catchment

Duration (hours)	Rainfall depth (mm)
3	98
6	138
9	170

Duration (hours)	Rainfall depth (mm)
12	197
18	245
24	287
36	367
48	417
72	474
96	501

Concrete gravity weir

Since the consequence category for the concrete gravity weir is **Significant**, a fallback flood capacity for was taken as 1:1,000 AEP based on ANCOLD (2000) adopting the lower end of the required range. It is assumed that the reservoir will not have any significant attenuation of the inflows due to the much reduced storage volume and that inflows are equal to outflows. The design inflow and outflow is 31.4m³/s.

Replacement Embankment

Arrangement

A replacement embankment was considered just downstream of the existing embankment. Drawings of the proposed dam can be found in Appendix A. The embankment has the following features:

- Height of the embankment: ~8m
- Upstream slope: 1V:3H
- Downstream slope: 1V:2.5H
- Embankment crest width: 4m
- Embankment crest level: RL 608.3m
- Spillway: 10m long x 2m deep concrete spillway with a broad crested weir around right abutment
- Spillway crest level: RL 606.3m
- Spillway chute: 91m long concrete chute discharging into natural river course
- Outlet work: Ø500mm concrete encased HDPE pipe with a Ø500mm gate valve

Embankment

Embankment crest level was worked out based on the wet freeboard requirements for 1:10,000 AEP flood event and adopting a 0.5m freeboard. Reservoir routing for 1:10,000 AEP flood event for the

adopted spillway gave a design flood level of RL 607.8m. Therefore, a final crest level of RL 608.3m was adopted.

The embankment adopted is an earthfill embankment with clay core and 2A filter. It is assumed that the earthfill required for the embankment can be sourced from the reservoir area. The clay core is assumed to be sourced locally. Only one filter, i.e. 2A, has been adopted for chimney filter on the downstream face of central clay core and will be placed between the clay core and the downstream earthfill. However, for blanket filter a 2B filter has also been considered, in addition to 2A filter for higher drainage capacity along the base of downstream earthfill.

The upstream and downstream slope of the embankment was adopted to be 1V:3H and 1V:2.5H respectively. Based on USBR (1987), small dams with proper drainage can have a downstream slope of 1V:2H to 1V:2.5H. Formal stability assessments for different loading conditions have not been undertaken but very limited geotechnical information is available on the site.

Protection of upstream face against wave generated erosion has been provided by incorporating a nominal 1m thick layer of riprap over geofabric for 2/3rd height of the dam from the crest.

Spillway

The full supply level of the replacement embankment has been kept. A free flowing broad crested spillway has been designed for 1:10,000 AEP flood. The dimensions were iterated for the peak outflow and the optimum length and depth were worked out. Based on this, final length and depth was fixed as 10m and 2m respectively allowing for a freeboard of 500mm at the crest.

The chute has a maximum slope of 8.2%. Based on this slope, depth of flow at different sections was worked out for the peak outflow during 1:10,000 AEP flood event. The calculated maximum depth of flow in the chute was 0.86m and adopted maximum height of chute walls on each side was 1.4m allowing for a freeboard of 500mm.

Energy dissipater

An energy dissipater structure has been provided at the end of the spillway chute. The dissipater is USBR Basin II type (USBR, 1986). The dimension of the dissipater is 7m x 10m x 2.1m (L x W x H).

Outlet

A 500mm diameter outlet conduit (HDPE, concrete encased) has been provided for new dam. The outlet meets the requirements for dewatering based on USBR (1990). Note that this does not take into account the inflow into the reservoir during dewatering operation. A trash rack on the head wall at the inlet of new outlet conduit has been included. Similarly, a head wall has been included at the exit. A gate valve (Ø500mm) just upstream of the head wall has also been incorporated in the design. The outlet will discharge slightly downstream of the spillway energy dissipater.

Instrumentation

As the dam is a **High C** consequence category dam, the following instruments have been incorporated in the design to comply with ANCOLD (2003):

- V-notch weir (x 1)
- Manually read reservoir level measuring gauge boards
- Dam deformation survey targets and benchmarks

It is assumed that daily rainfall data will be sourced from a nearby rain gauge via Bureau of Meteorology website.

Access to downstream area

A single lane vehicular bridge over the spillway to the spillway crest has been provided in the design. The adopted bridge is a precast concrete slab supported on spillway chute walls, which would be stiffened as necessary to carry the imposed loads.

Access to outlet works and dam toe is via the bridge over the spillway and crest leading to the left abutment track down to a vehicle parking area near the valve location. An access stairway has been incorporated from the parking area to the valve location.

Concrete Gravity Weir

Arrangement

A trapezoidal concrete gravity weir was considered just downstream of the existing embankment. Drawings of the proposed weir can be found in Appendix B. The concrete gravity weir has following features:

- Height of the weir: 4m from foundation level
- Upstream slope: Vertical
- Downstream slope: 1V:0.55H
- Crest width: 0.8m
- Abutment crest level: RL 604.5m
- Spillway: 27 m long x 1m deep central spillway discharging into an energy dissipater
- Spillway crest level: RL 603.5m
- Outlet: Ø500mm concrete encased HDPE pipe with Ø500mm gate valve

Weir

The parameters chosen for the global stability assessment were slightly conservative as no information is available on the foundation. The assumed parameters are presented below.

Table 2: Assumed parameters for stability assessment

Material	Parameter
Friction angle at rock/concrete interface	45°
Cohesion at rock/concrete interface	0 kPa
Concrete tensile strength at rock/concrete interface	0 kPa
Usual loading (assuming outlet is kept closed)	Reservoir level at 200mm above spillway crest

A suitable section was worked out using CADAM software. The factors of safety against sliding and overturning adopted for the stability analysis and the results obtained are as follows:

	Required FOS ¹			Analysed FOS		
	Usual loading	Unusual loading	Extreme loading	Usual loading	Unusual loading	Extreme loading
Sliding	3	2	1.5	3.1	2.6	1.8
Overturning	1.5	1.3	1.1	2.1	1.9	1.8

¹ANCOLD (2013) and CDA (2007)

Spillway

The spillway was designed for 1:1,000 AEP inflow. A free overflow broad crested weir spillway has been provided in the design. The dimensions were calculated for the peak outflow assuming there is no attenuation in the reservoir. Based on this, final length and depth was fixed as 27m and 1m respectively allowing for a freeboard of 200mm.

Height of the chute walls (0.5m) were determined based depth of flow for peak inflow. A freeboard of 200mm has also been allowed for.

Energy dissipater

An energy dissipater structure has been included at the end of the spillway chute. The dissipater is USBR Basin II type (USBR, 1986). The dimension of the dissipater is 11m x 20m x 1.52m (L x W x H).

Outlet

A 500mm diameter outlet conduit (HDPE, concrete encased) has been provided for the concrete gravity weir. The outlet meets the requirements for dewatering based on USBR (1990). Note that this does not take into account the inflow into the reservoir during dewatering operation. A trash rack with head wall at the inlet of new outlet conduit has been considered. Similarly, a head wall has been included at the exit with a valve just upstream of the head wall has also been incorporated.

Access to weir crest

No vehicular access has been provided for the weir crest.

Access to outlet valve

A single lane vehicular access to outlet valve at the toe of the weir has been provided from the right hand side abutment down to a parking area near the valve location.

Instrumentation

Instrumentation for concrete gravity weir has been incorporated based on the requirements for a **Significant** consequence category dam and are as follows:

- Manually read reservoir level measuring gauge boards
- Dam deformation survey targets and benchmark

It is assumed that daily rainfall data will be sourced from a nearby rain gauge via Bureau of Meteorology website.

Diversion during construction

The existing embankment would be used as a coffer dam during the construction of either replacement embankment or concrete gravity weir.

The existing embankment has a 400 mm diameter outlet conduit with a valve on the downstream side, which was recently refurbished. This conduit will be connected with the new outlet conduit (for replacement embankment as well as concrete gravity weir) to divert the inflows. Considering a construction flood equivalent to 10% percentile flow (i.e. flow that is not exceeded 90% of the time) which is equivalent to $1\text{m}^3/\text{s}$ (Pokharel, 2015), the combined capacity of the existing outlet pipe and the new outlet for replacement embankment and concrete gravity weir to divert the inflows was assessed. The maximum outflow that the conduit can discharge is $0.67\text{m}^3/\text{s}$ when the reservoir level is 300mm lower than the piping defect in the existing embankment. Therefore, there is a need to operate the existing spillway during construction of the replacement embankment and concrete gravity weir. The current crest level of the existing spillway is approximately RL 605.3m. Therefore, this existing spillway together with the outlet conduit can handle the construction flood.

Diversion for replacement embankment

At the preliminary stages of construction, the existing spillway will have to be used for diverting the inflows. Once the new outlet conduit is in place and connected to the existing outlet conduit, the combined outlet conduit will also be used for diverting the inflows. It should be noted that spillway wall on the left hand side at embankment interface and the spillway chutes will have to be constructed prior to construction of the embankment. This will have a couple of advantages:

- The new spillway can be used for diversion during embankment construction when inflows exceed the outlet capacity;
- Embankment can be compacted against the spillway wall at interface during construction.

The spillway crest wall (top RL of 606.3m) will have to be constructed at the end of construction work when the embankment works are complete.

A small earth and rockfill coffer dam will have to be constructed on the downstream side of the new embankment to protect the works area from back water inundation.

Diversion for concrete gravity weir

The existing spillway can be used for diverting inflows during construction. The existing spillway crest will have to be lowered slightly to prevent the existing embankment being overtopped during the weir construction.

A small coffer dam will have to be constructed on the downstream side of the concrete gravity weir to prevent the works area from back water.

Existing embankment

The existing embankment will have to be kept as is during construction of either the replacement embankment or concrete gravity weir. At the end of construction, the existing embankment will have to be lowered significantly and breached at the deepest section (around the existing outlet) so that water can flow to the replacement embankment or concrete gravity weir intake.

Divers will be required to install and remove a blank plate on the upstream side of the existing outlet conduit, so that this conduit can be connected and disconnected with the new conduit on the downstream side of the existing embankment.

Cost estimate

High level cost estimates (-10% to +30%) for the replacement embankment and concrete gravity weir have been undertaken. Details can be found in Appendix C. A summary of cost estimates is presented below:

Table 1: Cost estimate for replacement embankment (-10% to +30%)

Item	Cost
Preliminaries	\$106,000
Excavation work	\$494,000
Embankment construction	\$1,145,000
Spillway and energy dissipater	\$775,000
Instrumentation (telemetered V-notch weir, manual gauge boards and survey markers)	\$70,000
Engineering and project management	\$633,000
Sub-total	\$3,223,000
Contingency	\$557,000
Total	\$3,780,000

Table 2: Cost estimate for concrete gravity weir (-10% to +30%)

Item	Cost
Mobilisation, demobilisation and site preparation	\$82,000
Earthwork (excavation and removal or existing embankment)	\$233,000
Concrete gravity weir, spillway and energy dissipater	\$928,000
Instrumentation (manual gauge boards and survey markers)	\$31,000
Engineering and project management	\$351,000
Sub-total	\$1,625,000
Contingency	\$286,000
Total	\$1,911,000

Limitations

This report has been prepared based on the currently available information only to a high level concept design for indicative budgeting purposes. The following are noted as significant areas of uncertainty or risks that should be addressed prior to proceeding to feasibility study:

- The only geotechnical information available from site is the geological map of the area. Assumptions have been made that:
 - the local materials are suitable for construction and there is sufficient availability.
 - the permeability and strength at the assumed depth of the foundation is adequate for both options.
 - both of these issues would need to be proven by an appropriate level of geological and geotechnical investigation.
 - significant cost increases in construction cost estimate would occur if either or both of these risks were to eventuate.
- A detailed consequence category assessment for the proposed new dams have not been completed. A detailed assessment may lead to higher consequence categories, leading to higher design standards and increased construction cost estimate to meet these requirements (e.g. higher flood capacity).
- No assessment of the economics of either of the proposed new dams have been undertaken. TasWater should assess the benefits of this development.
- No consideration of potential environmental, cultural or aboriginal heritage impacts have been made.
- No consideration has been made of potential permit requirements may have on the dam design and hence potential construction cost impacts.

References

- ANCOLD (2000). *Guidelines on selection of acceptable flood capacity for dams*, Australian National Committee on Large Dams, March 2000.
- ANCOLD (2003). *Guidelines on dam safety management*, Australian National Committee on Large Dams, August 2003.
- ANCOLD (2013). *Guidelines on design criteria for concrete gravity dams*, Australian National Committee on Large Dams, September 2013.
- Ball J, Babister M, Nathan R, Weeks W, Weinmann E, Retallick M, Testoni I, (2016). *Australian rainfall and runoff: a guide to flood estimation*, © Commonwealth of Australia (Geoscience Australia), 2016.
- Bureau of Meteorology (2006). *Guidebook to the estimation of PMP: generalised southeast Australia method*, BOM, 2006.
- Bureau of Meteorology , 2003. *The estimation of probable maximum precipitation in Australia: generalised short-duration method*, BOM, 2003.
- CDA (2007). *Dam safety guidelines*, Canadian Dam Association, 2007.
- Cohen, W. & Southcott, P. (2018), *Waratah dam flood attenuation study draft report*, ENTURA-F1C8B Monday 30th April 2018.
- Jordan, P., Nathan, R., Mittiga, L. and Taylor, B. (2005). *Growth curves and temporal patterns of short duration design storms for extreme events*, Australian Journal of Water Resources, 9(1), pp69-80, 2005.
- Pokhrel, P. (2015). *Waratah River yield analysis*, Rev 0.1, ENTURA-95C6A, January 2015.
- USBR (1984). *Hydraulic design of stilling basins and energy dissipaters*, A water resources technical publication, Engineering monograph no. 25, United States Department of Interior Bureau of Reclamation, May 1984.
- USBR (1990). *Criteria and guidelines for evacuating storage reservoirs and sizing low-level outlet works*, ACER Technical Memorandum No.3, United States Bureau of Reclamation, 1990.

Software:

CADAM (2003), Version 1.4.12, Department of Civil, Geological and Mining Engineering, Montreal, Canada, 2003.

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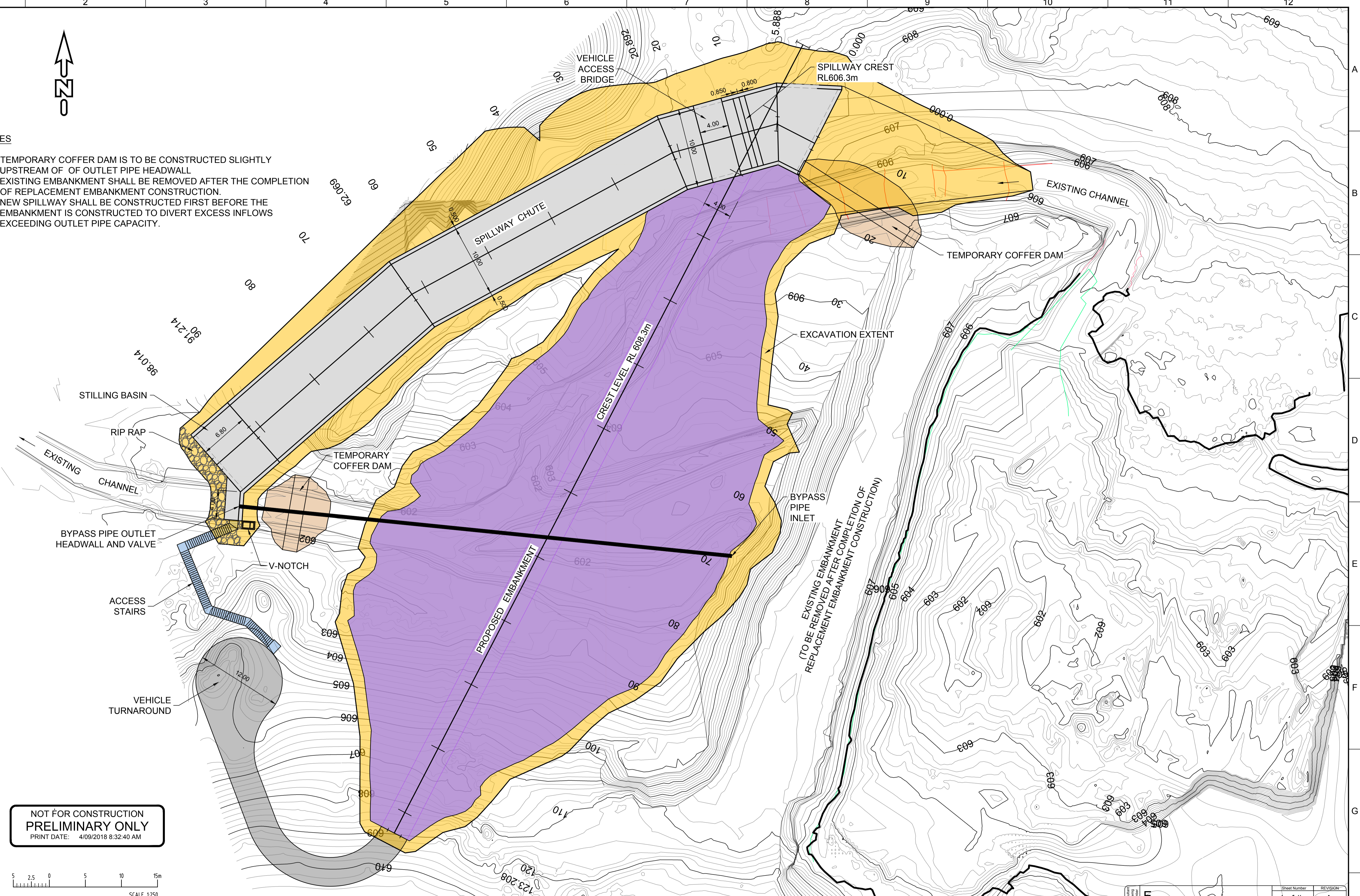
Appendix A – Embankment option drawings

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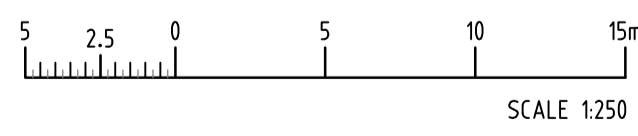


NOTES

1. TEMPORARY COFFER DAM IS TO BE CONSTRUCTED SLIGHTLY UPSTREAM OF OF OUTLET PIPE HEADWALL
2. EXISTING EMBANKMENT SHALL BE REMOVED AFTER THE COMPLETION OF REPLACEMENT EMBANKMENT CONSTRUCTION.
3. NEW SPILLWAY SHALL BE CONSTRUCTED FIRST BEFORE THE EMBANKMENT IS CONSTRUCTED TO DIVERT EXCESS INFLOWS EXCEEDING OUTLET PIPE CAPACITY.



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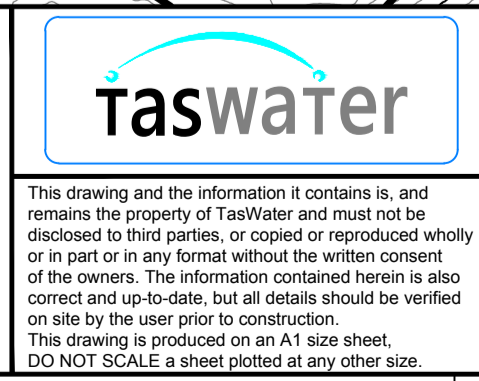


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Vault Folder	Projects	Designed	S.NEUPANE	04/09/2018
Discipline	C M E R	Verified	P.SOUTHCOTT	04/09/2018
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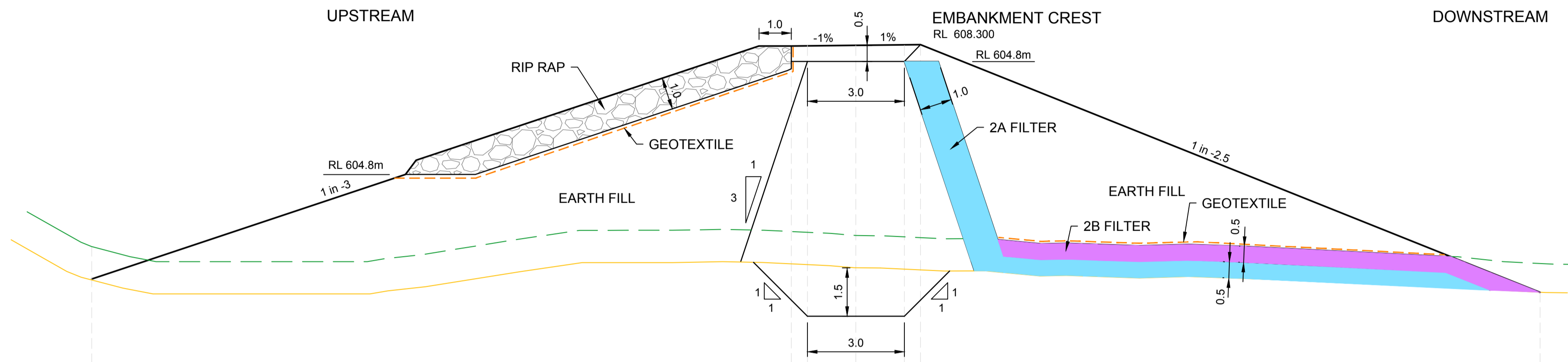


WARATAH DAM REPLACEMENT CONCEPT DESIGN EMBANKMENT AND SPILLWAY PLAN

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ABN: 47 162220 653

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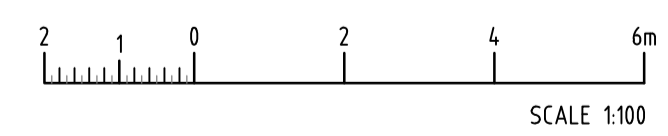


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EXISTING SURFACE	602.064	602.551	602.410	602.020	602.651
OFFSET	-23.649	-2.000	0.000	2.000	21.173

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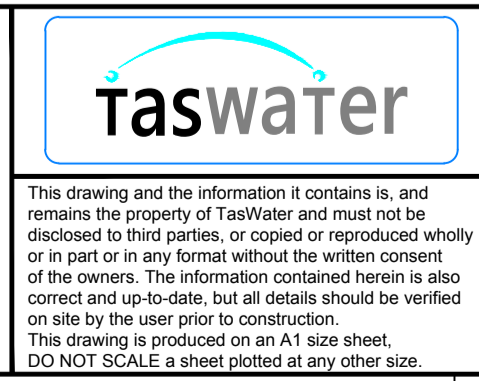
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Discipline	C M E R	Verified	P.SOUTHCOTT	04/09/2018
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WARATAH DAM REPLACEMENT CONCEPT DESIGN
EMBANKMENT
TYPICAL CROSS SECTION

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 ABN: 47 162220 653

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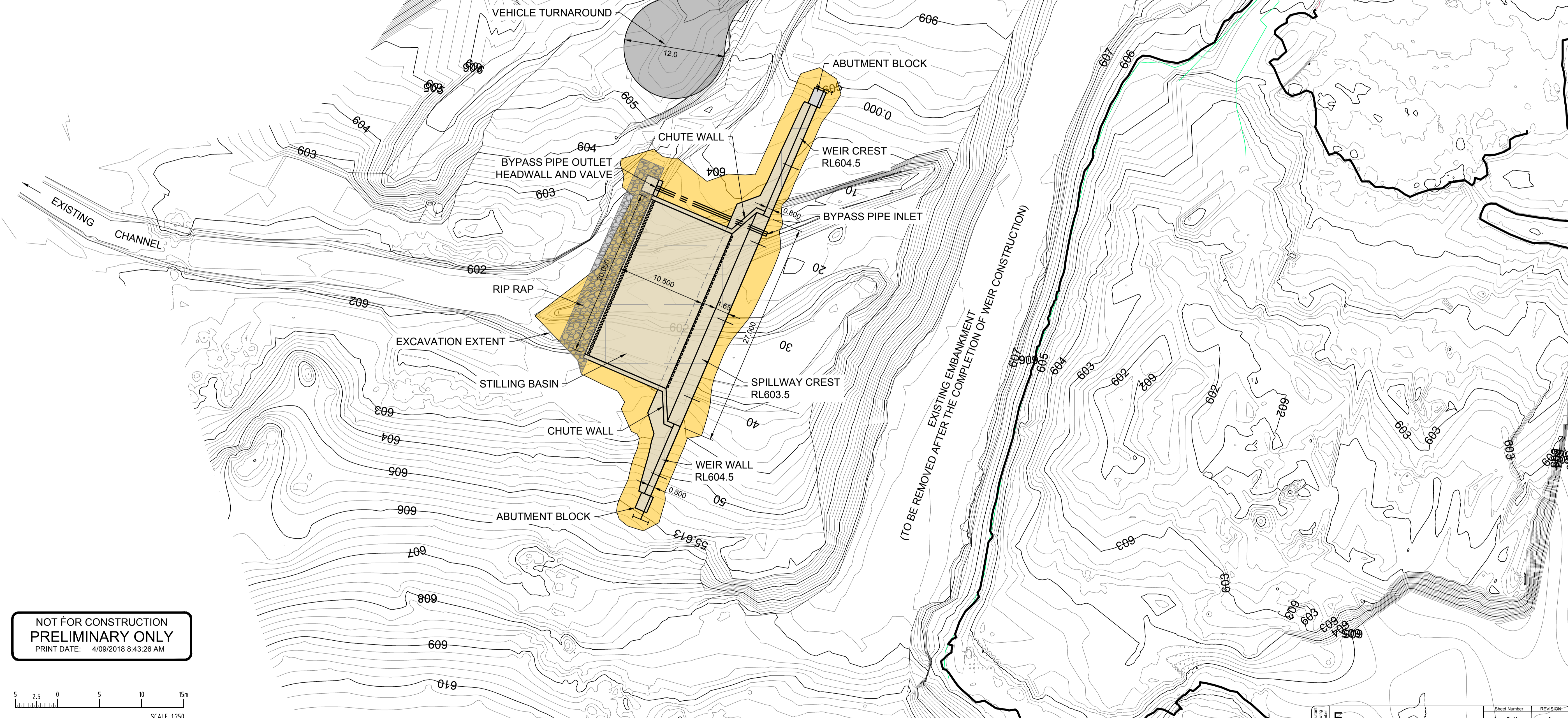
Appendix B – Concrete weir option drawings

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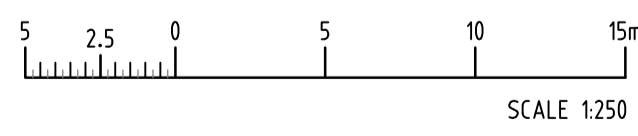


NOTES

1. EXISTING SPILLWAY CHANNEL SHALL BE USED AS A DIVERSION FOR FLOWS EXCEEDING OUTLET PIPE CAPACITY.
2. EXISTING EMBANKMENT SHALL BE REMOVED AFTER THE COMPLETION OF REPLACEMENT EMBANKMENT CONSTRUCTION.



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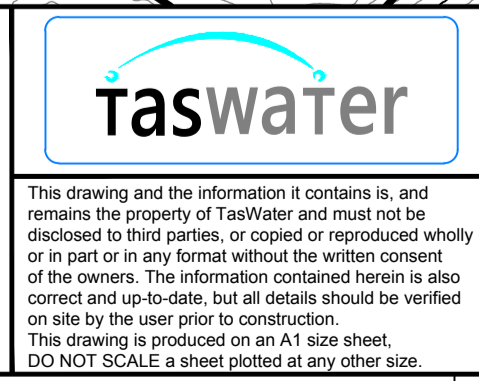


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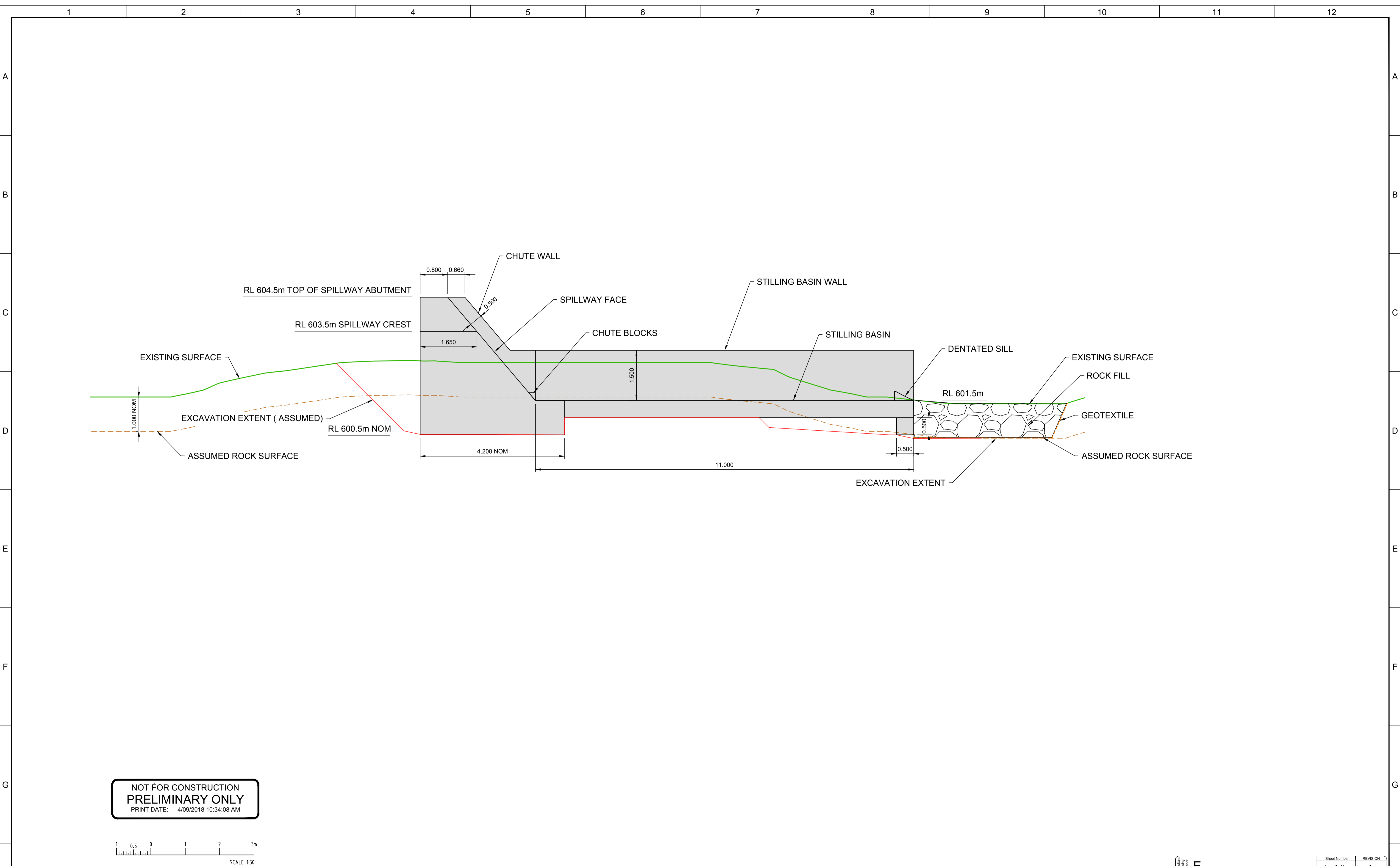


**WARATAH DAM REPLACEMENT CONCEPT DESIGN
CONCRETE GRAVITY WEIR AND SPILLWAY
PLAN**

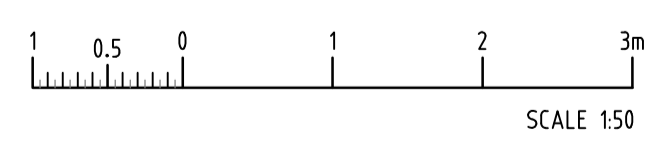
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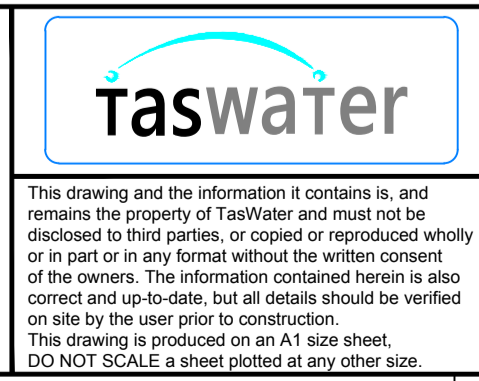


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Discipline	C M E R	Verified	P.SOUTHCOTT	04/09/2018
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**WARATAH DAM REPLACEMENT CONCEPT DESIGN
CONCRETE GRAVITY WEIR ENERGY DISSIPATOR
TYPICAL CROSS SECTION**

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Sheet Number	1 of #	REVISION	A
Drawing Number	P514459-CGW-002		

Sheet Number	1 of #	REVISION	A
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Appendix C – Cost estimates

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ENGINEERING ESTIMATING SERVICES

PAGE 1 OF 11

ESTIMATE SUMMARY SHEET -10% +30%

JOB No.P-514459

CLIENT: ENTURA

PROJECT: WARATAH DAM REPLACEMENT

REFERENCES: DRAWINGS & INFORMATION PROVIDED BY ENTURA PERSONNEL

OPTION 1 - EARTH FILL EMBANKMENT & CONCRETESPILLWAY

PRELIMINARIES	105,900
EXCAVATION WORK	494,000
NEW EARTHFILL EMBANKMENT	1,145,300
NEW CONCRETE SPILLWAY	774,700
INSTRUMENTATION	70,000
ENGINEERING & PROJECT MANAGEMENT	633,000
<u>BASIC TOTAL</u>	<u>3,222,900</u>

CONTINGENCY	557,100
ESCALATION - NOT CALCULATED	

TOTAL ESTIMATED COST OF OPTION 1 **\$3,780,000**

ESTIMATED COST RANGE FROM \$3,402,000 TO \$4,914,000

OPTION 2 - CONCRETE GRAVITY WEIR & SPILLWAY

PRELIMINARIES	82,270
EXCAVATION WORK	232,800
NEW CONCRETE GRAVITY WEIR & SPILLWAY	927,800
INSTRUMENTATION	31,500
ENGINEERING & PROJECT MANAGEMENT	351,000
<u>BASIC TOTAL</u>	<u>1,625,370</u>

CONTINGENCY	285,630
ESCALATION - NOT CALCULATED	

TOTAL ESTIMATED COST OF OPTION 2 **\$1,911,000**

ESTIMATED COST RANGE FROM \$1,720,000 TO \$2,484,000

ESTIMATED BY: J.HICKEY (E.E.S.)

DATE: 7-SEPTEMBER-2018

PROJECT / ESTIMATE No.P-514459			ESTIMATE SHEET			DATE: 07-Sep-18		PAGE 2 OF 11	
DESCRIPTION	SUMMARY		DES.VARIAT.	SUB TOTAL	CONTINGENCY		TOTAL COST	COMMENT	
	MATERIAL	LABOUR			%	AMOUNT			
OPTION 1 - EARTHFILL EMBANKMENT & CONCRETE SPILLWAY									
PRELIMINARIES	91,400	14,500	0	105,900	15	15,885	121,785		
EXCAVATION WORK	494,000	0	0	494,000	20	98,800	592,800		
NEW EARTHFILL EMBANKMENT	1,143,500	1,800	0	1,145,300	20	229,060	1,374,360		
NEW CONCRETE SPILLWAY	774,700	0	0	774,700	17.5	135,573	910,273		
INSTRUMENTATION	70,000	0	0	70,000	20	14,000	84,000		
ENGINEERING & PROJECT MANAGEMENT	58,000	575,000	0	633,000	10	63,300	696,300		
Contingency Adjustment						482			
BASIC TOTALS	2,631,600	591,300	0	3,222,900		557,100	3,780,000		
CONTINGENCY							INCLUDED		
ESCALATION - NOT CALCULATED							0		
TOTAL ESTIMATED COST OF OPTION 1							3,780,000		
OPTION 2 - CONCRETE GRAVITY WIER & SPILLWAY									
PRELIMINARIES	67,770	14,500	0	82,270	15	12,341	94,611		
EXCAVATION WORK	232,800	0	0	232,800	20	46,560	279,360		
NEW CONCRETE WEIR & SPILLWAY	926,000	1,800	0	927,800	20	185,560	1,113,360		
INSTRUMENTATION	31,500	0	0	31,500	20	6,300	37,800		
ENGINEERING & PROJECT MANAGEMENT	26,000	325,000	0	351,000	10	35,100	386,100		
Contingency Adjustment						-231			
BASIC TOTALS	1,284,070	341,300	0	1,625,370		285,630	1,911,000		
CONTINGENCY							INCLUDED		
ESCALATION - NOT CALCULATED							0		
TOTAL ESTIMATED COST OF OPTION 2							1,911,000		

PROJECT / ESTIMATE No.P-514459		ESTIMATE SHEET				DATE:	07-Sep-18	PAGE 4 OF 11	
DESCRIPTION	MATERIAL			COST	DAYS	LABOUR	TOTAL	COMMENT	
	QTY	UNIT	RATE			RATE			COST
OPTION 1									
Earthfill Embankment & Concrete Spillway (con't)									
EXCAVATION WORK									
Strip Embankment area - approx.3850m2 x 300mm depth	1200	m3	25	30,000	Included		0	30,000	JH Calc
Excavation to assumed rock level - approx 4400m2 x 500mm deep for Embankment	2200	m3	30	66,000	Included		0	66,000	JH Calc
Additional excavation for Embankment Toe - approx 105m length x 5m x 1.5m depth	800	m3	40	32,000	Included		0	32,000	JH Calc
Strip Spillway area - approx.2300m2 x 300mm depth	700	m3	25	17,500	Included		0	17,500	JH Calc
Excavation to assumed rock level - approx 2300m2 x ave 1.7m deep for Spillway	3950	m3	36	142,200	Included		0	142,200	JH Calc
Construct temporary Cofferdam at Spillway entry end - 20m long x 3m high x 8m wide ave	360	m3	30	10,800	Included		0	10,800	JH Calc
Construct temporary Cofferdam at Spillway discharge end	150	m3	30	4,500	Included		0	4,500	JH Calc
Remove Cofferdams after new Embankment & Spillways are constructed	550	m3	20	11,000	Included		0	11,000	JH Calc
Remove existing Embankment after new Embankment has been constructed - approx. 90m length x 16m wide x 4m ave high & dispose of rubble	6000	m3	30	180,000	Included		0	180,000	JH Calc
Sub Total - Excavation Work				494,000			0	494,000	

PROJECT / ESTIMATE No.P-514459		ESTIMATE SHEET				DATE:	07-Sep-18	PAGE 5 OF 11	
DESCRIPTION	QTY	MATERIAL		COST	DAYS	LABOUR	COST	TOTAL	COMMENT
		UNIT	RATE			RATE		COST	
OPTION 1									
Earthfill Embankment & Concrete Spillway (con't)									
NEW EARTHFILL EMBANKMENT									
Place new Core material - 100m length x 6m depth x 5.3m ave	3200	m3	55	176,000	Included		0	176,000	Ref Mikany dam
Place 2A Filter medium - 100m x 4m x 1000mm	400	m3	230	92,000	Included		0	92,000	Ref Mikany dam
Place 2A Filter medium - 100m x 15m x 500mm	750	m3	230	172,500	Included		0	172,500	Ref Mikany dam
Place 2B Filter medium - 100m x 16m x 500mm	800	m3	160	128,000	Included		0	128,000	Ref Mikany dam
Place Geotextile membrane between 2B Filter & Earthfill - 100m x 15m	1500	m2	10	15,000	Included		0	15,000	Ref Mikany dam
Place Earthfill - 270m x 17m x 2m average	3600	m3	80	288,000	Included		0	288,000	Ref Mikany dam
Place Geotextile membrane under Rip Rap on U/S face - 100m x 15m	1500	m2	12	18,000	Included		0	18,000	Ref Mikany dam
Place Rip Rap on U/S Face -100m x 11m x 1m deep	1100	m3	75	82,500	Included		0	82,500	Ref Mikany dam
Place & compact Gravel Road Base over Earthfill material & compact to RL 608.3 Approx. 4m wide x 500mm deep x 100m	200	m3	90	18,000	Included		0	18,000	Ref Mikany dam
Install new Bypass Pipe - 70m long x 500mm HDPE	70	m	500	35,000	Included		0	35,000	JH Calc
Mass concrete encase Bypass pipe	145	m3	400	58,000	Included		0	58,000	JH Calc
Isolation Gate Valve x 500mm dia	1	No	7,500	7,500	2	900	1,800	9,300	Emerson Budget
Outlet wall & apron	12	m3	1,500	18,000	Included		0	18,000	JH Calc
Construct vehicle access & turnaround area including excavation & preparation	250	m2	80	20,000	Included		0	20,000	JH Calc
Timber access stairs to valve location incl.timber ballastrade	25	m	600	15,000	Included		0	15,000	JH / Cordell
Sub Total - New Earthfill Embankment				1,143,500			1,800	1,145,300	

PROJECT / ESTIMATE No.P-514459		ESTIMATE SHEET				DATE:	07-Sep-18	PAGE 6 OF 11	
DESCRIPTION	QTY	MATERIAL		COST	DAYS	LABOUR	COST	TOTAL	COMMENT
		UNIT	RATE			RATE		COST	
OPTION 1									
Earthfill Embankment & Concrete Spillway (con't)									
NEW CONCRETE SPILLWAY									
Lay FCR or similar under new Spillway - 95m in length x 12m wide x 300mm deep	340	m3	80	27,200	Included		0	27,200	JH Calc
Spillway Crest & Entry slab	95	m3	1,100	104,500	Included		0	104,500	JH Calc
Spillway Channel invert slab	385	m3	900	346,500	Included		0	346,500	JH Calc
Spillway Channel walls - 95m x ave 1.3m high x 500mm thick incl.reo & formwork	125	m3	1,600	200,000	Included		0	200,000	JH Calc
Stilling Basin slab & end wall	40	m3	1,000	40,000	Included		0	40,000	JH Calc
Stilling Basin walls	20	m3	1,600	32,000	Included		0	32,000	JH Calc
Vehicle access Bridge - assume steel frame & concrete - 11m wide x 4m wide	1	Item	11,000	11,000	Included		0	11,000	JH Calc
Place Rip Rap at Stilling Basin end of Spillway approx. 100m2 x 500mm deep	50	m3	70	3,500	Included		0	3,500	JH Calc
New V-Notch Weir	1	Item	10,000	10,000	Included		0	10,000	JH Calc
<u>Sub Total - New Concrete Spillway</u>				<u>774,700</u>			<u>0</u>	<u>774,700</u>	
INSTRUMENTATION									
Allowance for Survey Targets & Flowmeter at V notch Weir,manual Gauge Board & Telemetry	1	Item	70,000	70,000	Included		0	70,000	JH Calc
<u>Sub Total - Instrumentation</u>				<u>70,000</u>			<u>0</u>	<u>70,000</u>	

PROJECT / ESTIMATE No.P-514459		ESTIMATE SHEET					DATE:	07-Sep-18	PAGE 11 OF 11	
DESCRIPTION	QTY	MATERIAL		COST	DAYS	LABOUR	COST	TOTAL	COMMENT	
		UNIT	RATE			RATE		COST		
OPTION 2										
Concrete Gravity Weir & Spillway (con't)										
INSTRUMENTATION										
Allowance for Survey Targets & Level Gauge at Weir	1	Item	31,500	31,500	Included		0	31,500	JH Calc	
Sub Total - Instrumentation				31,500			0	31,500		
ENGINEERING & PROJECT MANAGEMENT										
Engineering Design, Drafting, Geotech & Environmental Studies at 12.5% of Direct Costs - on \$1,561,000	1	Item	20,000	20,000			175,000	195,000	JH Fig	
Project Management, Site Supervision, Meetings, Contractor & Client Liaison at 10% of Direct Costs on \$1,275,000	1	Item	6,000	6,000			150,000	156,000	JH Fig	
Sub Total - Engineering & Project Management				26,000			325,000	351,000		

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